

* Advantages of welded connection :->

- 1) As no holes are required for welding the cis area of member is effective hence more effective in taking load.
 - 2) welded joint provide rigidity and strength.
 - 3) welded structures are comparatively lighter than bolted structure.
 - 4) A welded joint has better finish and appearance.
 - 5) welded joint are economical and less labour and material are required for joint.
 - 6) No noise is produce in the welding process.
 - 7) welded structure maintenance & painting are easy.
- * Disadvantage
- 1) welded connection required skill labour.
 - 2) without electricity you can't weld.
 - 3) Internal stresses and warping are produced due to uneven heating and cooling.
 - 4) It is difficult to inspect. aka pocket

incomplete penetration in welding.

5) Testing of welded joint is difficult.

Welded connections :->

There are two types of welded connections

- 1) butt weld or groove weld.
- 2) lap weld

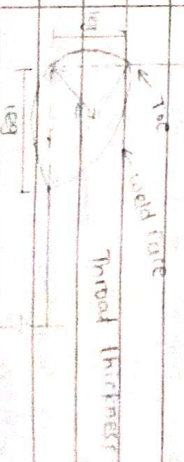
1) Butt weld or groove weld.

when the member is connected in a same plane butt weld are used.



2) lap weld

when the member is allowed to lap one over other lap welding is preferred.



* welded connection \Rightarrow

1) size of fillet weld \Rightarrow (s)
 size of normal fillet weld is taken equal to its minimum leg length.

a) minimum size

Thickness of thinner plate minimum size

- 1) upto 10 mm 3mm
- 2) 11 to 20 mm 5mm
- 3) 21 to 32 mm 6mm
- 4) 32 to 50 mm 10mm

b) maximum of size of fillet weld \Rightarrow

maximum size of fillet weld applied to a square edge of a plate of thickness above 4 mm should not exceed thickness of the edge minus 1.5.

square edge = $t - 1.5$ where $t =$ thickness of thinner plate

for rounded or rolled steel section, maximum size of fillet weld not exceed $\frac{3}{4} \times t$

rolled or rounded = $\frac{3}{4} \times t$ where, $t =$ thickness of rolled section

* Throat thickness (t_t) \Rightarrow

It is the perpendicular distance from the root of the fillet weld to the line joining its toe.

It is taken equal to $k \times$ size of fillet weld

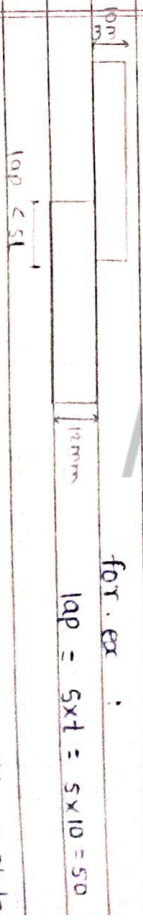
$t_t = k \times$ size of fillet weld.

The value of k is depend upon angle of fusion

Angle between fusion face	60-90°	91-100	101-106	107-113	114-120
k	0.7	0.65	0.6	0.55	0.5

In almost case value of $k = 0.7$

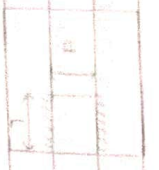
* overlap \Rightarrow The overlap in the lap joint should not be less than five time of thickness of thinner plate.



where $t =$ thickness of thinner plate

* side fillet or side weld \Rightarrow In a lap joint made by a side or longitudinal fillet weld the length of each fillet weld should not be

less than perpendicular distance between them



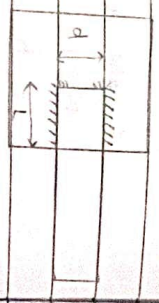
$l =$ not less than d
 $d =$ not exceed $16t$
 $d =$ width of plate.

* End returns \Rightarrow

fillet weld terminating at end of side of part of member should preferably be return continuously around the corner for a distance not less than twice the weld size.

End returns = $2 \times s$

$s =$ size of fillet weld.



* Problems of welding \Rightarrow

Type-1 : welding on three side

i) size of weld (S) \Rightarrow

ii) minimum size of weld :
 as per thickness is consider

iii) maximum size of weld :
 Square = $t - 1.5$
 Rolled section = $\frac{3 \times t}{4}$

where $t =$ thickness of thinner plate.

ii) throat thickness (H) :

$H = k \times s$ \textcircled{R} $H = 0.7 \times s$

iii) design stress of weld :

$$f_{wd} = \frac{F_u}{\sqrt{3} \times \gamma_{mw}}$$

γ_{mw} : 1) shop weld = $\gamma_{mw} = 1.25$

2) site weld = $\gamma_{mw} = 1.5$

If not given take $\gamma_{mw} = 1.5$

iv) strength of weld per mm length :

$$P_g = f_{ud} \times l \times t_t$$

v) factored load :

1) If P_{du} is given take same value.

2) If P_{du} is not given and length is given

$$P_{du} = f_{ud} \times l \times t_t$$

3) If P_{du} and length is not given and size of plate is given

$$P_{du} = \frac{A_g \times f_y}{\gamma_{mo}}$$

where

1) $A_g = b \times t$

2) $f_y = 250 \text{ N/mm}^2$

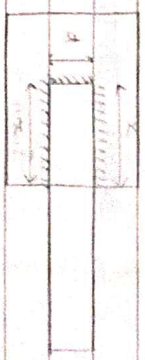
3) $\gamma_{mo} = 1.1$

vi) effective length of weld \Rightarrow

$$l_e = \frac{P_{du}}{P_g}$$

vii) End returns \Rightarrow End returns = $2 \times S$

viii) welding on three side :



$$l_e = x + d + x$$

$$l_e = 2x + d$$

$$l_e - d = 2x$$

$$x = \frac{l_e - d}{2}$$

where d = width of plate

Q.1)

calculate the lap of one plate having size $180 \times 10 \text{ mm}$. over other plate of size $180 \times 12 \text{ mm}$ transmit a pull of equal to full strength of smaller plate. assume fillet weld of 6 mm size and welding is operated on three side on the field. use yield stress as $f_y = 250 \text{ mpa}$. whereas ultimate stress as $f_u = 410$ in steel.

given data :

plate 1 = $120 \times 10 \text{ mm}$

plate 2 = $180 \times 12 \text{ mm}$

size of weld (S) = 6 mm

$f_y = 250 \text{ mpa}$

$f_u = 410 \text{ mpa}$

$\gamma_{mo} = 1.1$

welding on three side = ?

1) size of fillet weld (S) = 6 mm

2) throat thickness (tt) :

$$tt = k \times S = 0.7 \times 6$$

$$tt = 4.2 \text{ mm}$$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.5}$$

$$f_{wd} = 157.80 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{wd} \times l \times t_t = 157.80 \times 1 \times 4.2$$

$$P_q = 662.79 \text{ N/mm}$$

5) Factor load \rightarrow

$$P_{aw} = \frac{A_g \times f_y}{\gamma_{mo}} \quad \gamma_{mo} = 1.1$$

$$P_{aw} = \frac{120 \times 10^3 \times 250}{1.1}$$

$$P_{aw} = 272.72 \times 10^3 \text{ N}$$

6) effective length (l_e) :

$$l_e = \frac{P_{aw}}{P_q} = \frac{272.72 \times 10^3}{662.79}$$

$$l_e = 411.48 \text{ mm}$$

$$[l_e \approx 420 \text{ mm}]$$

7) End returns = $2 \times 5 = 2 \times 6 = 12 \text{ mm}$

8) welding on three side

$$l_e = x + d + x$$

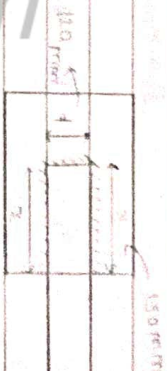
$$420 = x + 120 + x$$

$$420 - 120 = 2x$$

$$300 = 2x$$

$$x = \frac{300}{2}$$

$$[x = 150 \text{ mm}]$$



Q.2)

a 80 x 8 mm plate is to be connected to a 120 x 8 mm plate in a lap joint to transmit factored pull of 125 kN. use 6 mm size weld calculate weld on three side.

given data :

$$\text{plate 1} = 80 \times 8 \text{ mm}$$

$$\text{plate 2} = 120 \times 8 \text{ mm}$$

$$P_{aw} = 125 \text{ kN} = 125 \times 10^3 \text{ N}$$

$$S = 6 \text{ mm}$$

1) size of weld (S) = 6 mm

2) throat thickness (t_t) :

$$t_t = K \times S = 0.7 \times 6$$

$$t_t = 4.2$$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.5}$$

$$f_{wd} = 157.80 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{wd} \times l \times t_f = 157.80 \times 1 \times 4.2$$

$$P_q = 662.79 \text{ N/mm}$$

5) factored load :

$$P_{dw} = 125 \times 10^3 \text{ N}$$

6) effective length (l_e) :

$$l_e = \frac{P_{dw}}{P_q} = \frac{125 \times 10^3}{662.79}$$

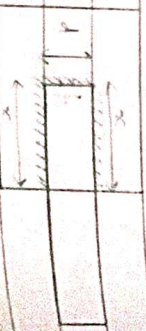
$$l_e = 188.59 \text{ mm}$$

$$[l_e \leq 200 \text{ mm}]$$

7) welding on three side :

$$x = \frac{l_e - d}{2} = \frac{200 - 80}{2}$$

$$x = 60 \text{ mm}$$



As $x = 60 \text{ mm}$ is less than $d = 80 \text{ mm}$
So we can't provide $x = 60 \text{ mm}$

Provide $x = 100 \text{ mm}$

3) design a suitable fillet weld of size 4 mm to connect a tie bar $80 \times 8 \text{ mm}$ to 10 mm thick gusset plate. Joint has to be design for full strength of the tie bar and welding on all three sides. take $f_y = 250 \text{ mpa}$, $\gamma_{mo} = 1$, $f_u = 410 \text{ mpa}$, and $\gamma_{mw} = 1.5$ draw a neat sketch showing lap length.

given data :

$$S = 4 \text{ mm}$$

$$\text{plate size} = 80 \times 8 \text{ mm}$$

$$\text{thickness} = 10 \text{ mm}$$

$$f_y = 250 \text{ mpa}$$

$$\gamma_{mo} = 1.1$$

$$f_u = 410 \text{ mpa}$$

$$\gamma_{mw} = 1.5$$

welding on three side = ?

1) size of weld (S) = 4 mm

2) throat thickness (t_t) :

$$t_t = K \times S = 0.7 \times 4$$

$$t_t = 2.8 \text{ mm}$$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.5}$$

$$f_{wd} = 157.80 \text{ N/mm}^2$$

4) strength of weld per mm length : \rightarrow

$$P_q = f_{wd} \times l \times t_l = 157.80 \times 1 \times 2.8$$

$$P_q = 441.84 \text{ N/mm}$$

5) factored load :

$$P_{dw} = \frac{P_q \times \gamma_{Fg}}{\gamma_{mb}} = \frac{80 \times 8 \times 250}{1.1}$$

$$P_{dw} = 145.45 \times 10^3 \text{ N}$$

6) effective length (l_e)

$$l_e = \frac{P_{dw}}{P_q} = \frac{145.45 \times 10^3}{441.84}$$

$$l_e = 329.49 \text{ mm}$$

$$[l_e \approx 340 \text{ mm}]$$

7) welding on three side.

$$l_e = x + d + x$$

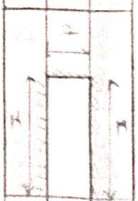
$$340 = 2x + 90$$

$$340 - 90 = 2x$$

$$2x = 260$$

$$x = \frac{260}{2}$$

$$[x = 130 \text{ mm}]$$



4) Find safe load transmitted by fillet weld between a flat 60 mm wide over lapping 100 mm over gusset plate. thickness of both plate is 10 mm. where is on all side of overlap. size of weld is 6 mm. which is provided at shop.

given data :

$$\text{Plate 1} = 60 \times 10 \text{ mm}$$

$$\text{Plate 2} = 100 \times 10 \text{ mm}$$

$$\text{thickness} = 10 \text{ mm}$$

$$S = 6 \text{ mm}$$

$$\text{welding at shop : } \gamma_{mw} = 1.25$$

1) size of weld (S) = 6 mm

2) throat thickness (t_t) :

$$t_t = K \times S = 0.7 \times 6$$

$$t_t = 4.2 \text{ mm}$$

3) design stress of weld

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.25}$$

$$f_{wd} = 189.37 \text{ N/mm}^2$$

4) strength of weld per mm length

$$P_q = f_{wd} \times 1 \times t = 189.37 \times 1 \times 4.2$$

$$P_q = 795.35 \text{ N/mm}$$

5) factor load :

$$P_{du} = P_q \times 1 \times t \quad L = 60 + 60 = 120 \text{ mm}$$

$$P_{du} = 189.37 \times 120 \times 4.2$$

$$P_{du} = 95.44 \times 10^3 \text{ N}$$

$$e) \text{ safe load} = \frac{P_{du}}{1.5} = \frac{95.44 \times 10^3}{1.5}$$

$$= 63.62 \times 10^3 \text{ N}$$

$$\text{Safe load} = 63.62 \text{ kN}$$

Type - 2 : Find longitudinal weld

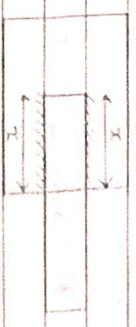
7 steps are same as type 1

8) welding on longitudinal side :

$$l_e = \alpha + x$$

$$l_e = 2x$$

$$\alpha = \frac{l_e}{2}$$



1) plate 150x10 mm is connected by 8 mm fillet weld. find lap required to be provided for longitudinal weld only. draw neat sketch showing lap length take $f_u = 410 \text{ MPa}$

given data :

plate size = 150x10 mm

$$S = 8 \text{ mm}$$

$$f_u = 410 \text{ MPa}$$

longitudinal weld = ?

1) size of weld (S) = 8 mm

2) throat thickness (H) :

$$H = K \times S = 0.7 \times 8$$

$$H = 5.6 \text{ mm}$$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.5}$$

$$f_{wd} = 157.80 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{wd} \times l \times t = 157.80 \times 1 \times 5.6$$

$$P_q = 883.73 \text{ N/mm}$$

5) factor load :

$$P_{ud} = \frac{P_q \times \gamma_f}{\gamma_{mo}} = \frac{150 \times 10^3 \times 250}{1.1}$$

$$P_{ud} = 340.90 \times 10^3 \text{ N}$$

6) effective length : →

$$l_e = \frac{P_{ud}}{P_q} = \frac{340.90 \times 10^3}{883.73}$$

$$l_e = 385.76 \text{ mm}$$

$$l_e \leq 400 \text{ mm}$$

7) End returns = $0 \times 5 = 2 \times 8 = 16 \text{ mm}$

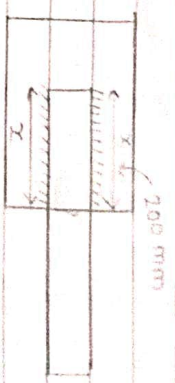
8) welding on longitudinal side :

$$l_e = x + x$$

$$l_e = 2x$$

$$\frac{400}{2} = x$$

$$[x = 200 \text{ mm}]$$



2) A 100 mm wide and 12 mm thick the plate has been connected to a gusset plate by 10 mm fillet weld. the lap of the plate over gusset plate is 120 mm. fillet weld has been done on two longitudinal edge and not at end. find out strength fillet weld joint.

given data :

plate size = $100 \times 12 \text{ mm}$

$S = 10 \text{ mm}$

length (L) = 120 mm

1) size of weld (S) = 10 mm

2) throat thickness (tt) :

$$tt = K \times S = 0.7 \times 10$$

$$tt = 7 \text{ mm}$$

3) design stress of weld :

$$f_{ud} = \frac{f_u}{\sqrt{3} \times 5 \text{ mm}} = \frac{410}{\sqrt{3} \times 1.5}$$

$$f_{ud} = 157.80 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{ud} \times l \times t = 157.80 \times 1 \times 7$$

$$P_q = 1104.66 \text{ N/mm}$$

5) factor load :

$$P_{du} = f_{ud} \times l \times t$$

$$P_{du} = 157.80 \times (120 + 120) \times 7$$

$$P_{du} = 265.104 \times 10^3 \text{ N}$$

6) effective length (l_e)

$$l_e = \frac{P_{du}}{P_q} = \frac{265.104 \times 10^3}{1104.66}$$

$$l_e = 239.98 \text{ mm}$$

$$l_e \approx 240 \text{ mm}$$

7) End returns : $2 \times 5 = 2 \times 10 = 20 \text{ mm}$

8) welding on longitudinal side :

$$l_e = x + x$$

$$240 = 2x$$

$$x = \frac{240}{2}$$

$$[x = 120 \text{ mm}]$$

9) safe load = $\frac{P_{du}}{1.5} = \frac{265.104 \times 10^3}{1.5}$

$$\text{safe load} = 176.73 \times 10^3 \text{ N}$$

$$[\text{safe load} = 176.73 \text{ kN}]$$

Type-3 : welding on three side and C_{se} is given.

1) design a suitable fillet weld connection for

ISA 480x50x8 with its longer leg connected to gusset plate of thickness 8 mm. the angle is subjected to factor load of 275 kN. take

$C_{xx} = 27.3$. Assume welding is applied to two edges and shop welding. $f_y = 250 \text{ MPa}$

$$f_u = 410$$

given data :

ISA = 80x50x8 mm

gusset plate thickness = 8 mm

$$P_{du} = 275 \text{ kN} \\ = 275 \times 10^3 \text{ N}$$

$$C_{ax} = 27.3$$

$$C_{gy} = 250 \text{ mPa}$$

$$f_u = 410 \text{ mPa}$$

$$\text{Shop weld } \delta_{mw} = 1.25$$

1) size of weld (s) :

minimum size of weld = 3 mm

$$\text{maximum size of weld } (\delta_{max}) = \frac{3}{4} \times t = \frac{3}{4} \times 8$$

$$\delta_{max} = 6 \text{ mm}$$

provide [S = 5 mm]

$$2) \text{ throat thickness } (t_t) = k \times S = 0.7 \times 5 \\ = 3.5 \text{ mm}$$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.25}$$

$$f_{wd} = 189.37 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{wd} \times l \times t_t = 189.37 \times 1 \times 3.5$$

$$P_q = 662.79 \text{ N/mm}$$

5) factored load :

$$P_{du} = 275 \times 10^3 \text{ N}$$

6) effective length (l_e) :

$$l_e = \frac{P_{du}}{P_q} = \frac{275 \times 10^3}{662.79}$$

$$l_e = 414.91 \text{ mm}$$

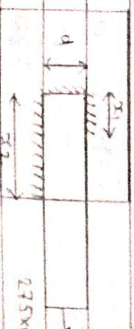
$$l_e \approx 430 \text{ mm}$$

7) End returns = 2x5 = 2x5 = 10 mm

8) welding on three side and C_{ax} is given :

$$P_{qx} \times l \times d + P_{qy} \times d \times \frac{d}{2} - (P_{du} \times C_{ax}) = 0$$

$$662.79 \times 10^3 \times 80 \times 80 + 662.79 \times 80 \times 80 \times \frac{80}{2} - (275 \times 10^3 \times 27.3) = 0$$



$$53.02 \times 10^3 \times 2 \times 1 - 5.386 \times 10^6 = 0$$

$$53.02 \times 10^3 \times 2 \times 1 = 5.386 \times 10^6$$

$$x_1 = \frac{5.386 \times 10^6}{53.02 \times 10^3}$$

$$x_1 = 101.58 \text{ mm}$$

$$[x_1 \cong 110 \text{ mm}]$$

$$e = x_1 + d + x_2$$

$$x_2 = e - x_1 - d$$

$$x_2 = 430 - 110 - 80$$

$$[x_2 = 240 \text{ mm}]$$

- 2) calculate the length of fillet weld required to connect ISN. 100x100x10. with gusset plate 6mm. weld as shown in figure. the angle is subjected to factored axial force 300kN c_{yx} and c_{yy} is 28.4 mm



Given data :

$$\text{ISN} = 100 \times 100 \times 10 \text{ mm}$$

Thickness of gusset weld = 6mm

$$P_d = 300 \text{ kN} = 300 \times 10^3 \text{ N}$$

$$c_{yx} = c_{yy} = 28.4 \text{ mm}$$

$$f_u = 410 \text{ N/mm}^2$$

$$f_y = 250 \text{ N/mm}^2$$

1) size of fillet weld (S) :

minimum size of weld (S_{\min}) = 3mm

maximum size of weld (S_{\max}) = $\frac{3}{4} \times t$

$$= \frac{3}{4} \times 10$$

$$S_{\max} = 7.5 \text{ mm}$$

Provide [S = 6 mm]

2) throat thickness (tt) = $k \times S = 0.7 \times 6$

$$tt = 4.2 \text{ mm}$$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.5}$$

$$f_{wd} = 157.80 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{wd} \times tt = 157.80 \times 4.2$$

$$P_q = 662.76 \text{ N/mm}$$

5) factored load (P_d) = $300 \times 10^3 \text{ N}$

6) effective length (le) =

$$I_e = \frac{P d w}{P q} = \frac{300 \times 10^3}{662.76}$$

$$I_e = 452.65 \text{ mm}$$

$$I_e \approx 460 \text{ mm}$$

7) End Returns = $2 \times 5 = 2 \times 6 = 12 \text{ mm}$

8) welding on three side & cor & cys is given



$$(P q x_1 x d) + \left(P q x d x \frac{d}{2} \right) - (P d w x c o r x) = 0$$

$$(662.76 \times x_1 \times 100) + \left(662.76 \times 100 \times \frac{100}{2} \right) - (300 \times 10^3 \times 28.4) = 0$$

$$662.76 x_1 - 5.206 \times 10^6 = 0$$

$$662.76 x x_1 = 5.206 \times 10^6$$

$$x_1 = \frac{5.206 \times 10^6}{662.76}$$

$$x_1 = 78.55 \text{ mm}$$

$$x_1 = 800 \text{ mm}$$

3.3]

ISA ~~80~~ 100x100x10 is welded with gusset plate of 12 mm. to carry factored pull of 300 kN. add its centroid 28 mm from outstanding leg. design fillet weld only on both side of weld angle. assume $f_e = 410$ & shop weld.

given data "

$$I S A = 100 \times 100 \times 10 \text{ mm}$$

thickness of gusset plate = 12 mm.

$$P d w = 300 \text{ kN} = 300 \times 10^3 \text{ N}$$

$$c o r = 28 \text{ mm}$$

$$f_u = 410 \text{ N/mm}^2$$

$$\delta m w = 1.15$$

1) size of weld :

minimum size of weld (S_{min}) = 3 mm
maximum size of weld (S_{max}) = $\frac{3}{4} \times t$

$$= \frac{3}{4} \times 10$$

$$S_{max} = 7.5 \text{ mm}$$

provide $[s = 6 \text{ mm}]$

throat thickness $(t_f) = k \times s = 0.7 \times 6$
 $t_f = 4.2 \text{ mm}$

3) design stress of weld :

$$f_{wd} = \frac{f_u}{\sqrt{3} \times \gamma_{mw}} = \frac{410}{\sqrt{3} \times 1.25}$$

$$f_{wd} = 189.37 \text{ N/mm}^2$$

4) strength of weld per mm length :

$$P_q = f_{wd} \times l \times t_f = 189.37 \times 1 \times 4.2$$

$$P_q = 795.35 \text{ N/mm}$$

5) factored load :

$$P_{dw} = 300 \times 10^3 \text{ N}$$

6) effective length :

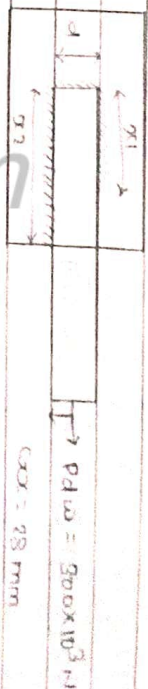
$$l_e = \frac{P_{dw}}{P_q} = \frac{300 \times 10^3}{795.35}$$

$$l_e = 377.19 \text{ mm}$$

$$l_e \leq 390 \text{ mm}$$

7) End Returns = $5 \times 2 = 2 \times 6 = 12 \text{ mm}$

8) welding on three side & case is given :



$$(P_q \times \alpha_1 \times d) + (P_q \times d \times \frac{d}{2}) - (P_{dw} \times c_{ax}) = 0$$

$$(795.35 \times \alpha_1 \times 100) + (795.35 \times 100 \times \frac{100}{2}) - (300 \times 10^3 \times 28) = 0$$

$$79535 \alpha_1 - 4.42 \times 10^6 = 0$$

$$79535 \alpha_1 = 4.42 \times 10^6$$

$$\alpha_1 = \frac{4.42 \times 10^6}{79535}$$

$$\alpha_1 = 55.57 \approx 60 \text{ mm}$$

$$l_e = \alpha_1 + d + \alpha_2$$

$$390 = 60 + 100 + \alpha_2$$

$$390 - 160 = \alpha_2$$

$$[\alpha_2 = 230]$$